

Formulae Booklet - OCR (A) Further Maths A-level

Advan

(H245)

Further Mathematics A

Formulae Booklet

The information in this booklet is for the use of candidates following the Advanced GCE in Further Mathematics A (H245) course.

The formulae booklet will be printed for distribution with the examination papers.

Copies of this booklet may be used for teaching.

This document consists of 16 pages.

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Pure Mathematics

Arithmetic series

$$S_n = \frac{1}{2}n(a+l) = \frac{1}{2}n\{2a+(n-1)d\}$$

Geometric series

$$S_n = \frac{a(1-r^n)}{1-r}$$
$$S_{\infty} = \frac{a}{1-r} \text{ for } |r| < 1$$

Binomial series

$$(a+b)^{n} = a^{n} + {}^{n}C_{1}a^{n-1}b + {}^{n}C_{2}a^{n-2}b^{2} + \dots + {}^{n}C_{r}a^{n-r}b^{r} + \dots + b^{n} \quad (n \in \mathbb{N}),$$

where ${}^{n}C_{r} = {}_{n}C_{r} = {\binom{n}{r}} = \frac{n!}{r!(n-r)!}$
$$(1+x)^{n} = 1 + nx + \frac{n(n-1)}{2!}x^{2} + \dots + \frac{n(n-1)\dots(n-r+1)}{r!}x^{r} + \dots \quad (|x| < 1, n \in \mathbb{R})$$

Series

$$\sum_{r=1}^{n} r^{2} = \frac{1}{6}n(n+1)(2n+1), \ \sum_{r=1}^{n} r^{3} = \frac{1}{4}n^{2}(n+1)^{2}$$

Maclaurin series

$$f(x) = f(0) + f'(0)x + \frac{f''(0)}{2!}x^2 + \dots + \frac{f^{(r)}(0)}{r!}x^r + \dots$$

$$e^x = \exp(x) = 1 + x + \frac{x^2}{2!} + \dots + \frac{x^r}{r!} + \dots \text{ for all } x$$

$$\ln(1+x) = x - \frac{x^2}{2} + \frac{x^3}{3} - \dots + (-1)^{r+1}\frac{x^r}{r} + \dots (-1 < x \le 1)$$

$$\sin x = x - \frac{x^3}{3!} + \frac{x^5}{5!} - \dots + (-1)^r \frac{x^{2r+1}}{(2r+1)!} + \dots \text{ for all } x$$

$$\cos x = 1 - \frac{x^2}{2!} + \frac{x^4}{4!} - \dots + (-1)^r \frac{x^{2r}}{(2r)!} + \dots \text{ for all } x$$

$$(1+x)^n = 1 + nx + \frac{n(n-1)}{2!}x^2 + \dots + \frac{n(n-1)\dots(n-r+1)}{r!}x^r + \dots \quad (|x| < 1)$$

Matrix transformations

Reflection in the line $y = \pm x : \begin{pmatrix} 0 & \pm 1 \\ \pm 1 & 0 \end{pmatrix}$

Anticlockwise rotation through θ about $O: \begin{pmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{pmatrix}$

1, $n \in \mathbb{R}$)

Rotations through θ about the coordinate axes. The direction of positive rotation is taken to be anticlockwise when looking towards the origin from the positive side of the axis of rotation.

$$\mathbf{R}_{x} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\theta & -\sin\theta \\ 0 & \sin\theta & \cos\theta \end{bmatrix}$$
$$\mathbf{R}_{y} = \begin{bmatrix} \cos\theta & 0 & \sin\theta \\ 0 & 1 & 0 \\ -\sin\theta & 0 & \cos\theta \end{bmatrix}$$
$$\mathbf{R}_{z} = \begin{bmatrix} \cos\theta & -\sin\theta & 0 \\ \sin\theta & \cos\theta & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Differentiation

f(x)	f'(x)
tan kx	$k \sec^2 kx$
sec x	$\sec x \tan x$
$\cot x$	$-\operatorname{cosec}^2 x$
cosec x	$-\csc x \cot x$
$\arcsin x$ or $\sin^{-1} x$	$\frac{1}{\sqrt{1-x^2}}$
$\arccos x \text{ or } \cos^{-1} x$	$-\frac{1}{\sqrt{1-x^2}}$
$\arctan x$ or $\tan^{-1} x$	$\frac{1}{1+x^2}$

Quotient rule $y = \frac{u}{v}, \ \frac{dy}{dx} = \frac{v\frac{du}{dx} - u\frac{dv}{dx}}{v^2}$

Differentiation from first principles

$$f'(x) = \lim_{h \to 0} \frac{f(x+h) - f(x)}{h}$$

Integration

$$\int \frac{f'(x)}{f(x)} dx = \ln|f(x)| + c$$
$$\int f'(x) (f(x))^n dx = \frac{1}{n+1} (f(x))^{n+1} + c$$

Integration by parts $\int u \frac{\mathrm{d}v}{\mathrm{d}x} \mathrm{d}x = uv - \int v \frac{\mathrm{d}u}{\mathrm{d}x} \mathrm{d}x$

The mean value of f(x) on the interval [a, b] is $\frac{1}{b-a} \int_a^b f(x) dx$

Area of sector enclosed by polar curve is $\frac{1}{2}\int r^2 d\theta$

f(x)	$\int \mathbf{f}(x)\mathrm{d}x$
$\frac{1}{\sqrt{a^2 - x^2}}$	$\sin^{-1}\left(\frac{x}{a}\right) (x < a)$
$\frac{1}{a^2 + x^2}$	$\frac{1}{a} \tan^{-1} \left(\frac{x}{a} \right)$
$\frac{1}{\sqrt{a^2 + x^2}}$	$\sinh^{-1}\left(\frac{x}{a}\right)$ or $\ln(x + \sqrt{x^2 + a^2})$
$\frac{1}{\sqrt{x^2 - a^2}}$	$\cosh^{-1}\left(\frac{x}{a}\right)$ or $\ln(x + \sqrt{x^2 - a^2})$ $(x > a)$

Numerical methods

Trapezium rule: $\int_{a}^{b} y \, dx \approx \frac{1}{2}h\{(y_0 + y_n) + 2(y_1 + y_2 + \dots + y_{n-1})\}, \text{ where } h = \frac{b-a}{n}$

The Newton-Raphson iteration for solving f(x) = 0: $x_{n+1} = x_n - \frac{f(x_n)}{f'(x_n)}$

Complex numbers

Circles: |z-a| = k

Half lines: $\arg(z-a) = \alpha$

Lines: |z - a| = |z - b|

De Moivre's theorem: $\{r(\cos \theta + i \sin \theta)\}^n = r^n(\cos n\theta + i \sin n\theta)$

Roots of unity: The roots of $z^n = 1$ are given by $z = \exp\left(\frac{2\pi k}{n}i\right)$ for k = 0, 1, 2, ..., n-1

Vectors and 3-D coordinate geometry

Cartesian equation of the line through the point A with position vector $\mathbf{a} = a_1 \mathbf{i} + a_2 \mathbf{j} + a_3 \mathbf{k}$ in direction

$$\mathbf{u} = u_1 \mathbf{i} + u_2 \mathbf{j} + u_3 \mathbf{k}$$
 is $\frac{x - a_1}{u_1} = \frac{y - a_2}{u_2} = \frac{z - a_3}{u_3} (= \lambda)$

Cartesian equation of a plane $n_1x + n_2y + n_3z + d = 0$

Vector product:
$$\mathbf{a} \times \mathbf{b} = \begin{pmatrix} a_1 \\ a_2 \\ a_3 \end{pmatrix} \times \begin{pmatrix} b_1 \\ b_2 \\ b_3 \end{pmatrix} = \begin{vmatrix} \mathbf{i} & a_1 & b_1 \\ \mathbf{j} & a_2 & b_2 \\ \mathbf{k} & a_3 & b_3 \end{vmatrix} = \begin{pmatrix} a_2b_3 - a_3b_2 \\ a_3b_1 - a_1b_3 \\ a_1b_2 - a_2b_1 \end{pmatrix}$$

The distance between skew lines is $D = \frac{|(\mathbf{b} - \mathbf{a}) \cdot \mathbf{n}|}{|\mathbf{n}|}$, where **a** and **b** are position vectors of points on each line and **n** is a mutual perpendicular to both lines

The distance between a point and a line is $D = \frac{|ax_1 + by_1 - c|}{\sqrt{a^2 + b^2}}$, where the coordinates of the point are (x_1, y_1) and the equation of the line is given by ax + by = c

The distance between a point and a plane is $D = \frac{|\mathbf{b} \cdot \mathbf{n} - p|}{|\mathbf{n}|}$, where **b** is the position vector of the point and the equation of the plane is given by $\mathbf{r} \cdot \mathbf{n} = p$

Small angle approximations

 $\sin\theta \approx \theta$, $\cos\theta \approx 1 - \frac{1}{2}\theta^2$, $\tan\theta \approx \theta$ where θ is small and measured in radians

Trigonometric identities

 $\sin(A \pm B) = \sin A \cos B \pm \cos A \sin B$ $\cos(A \pm B) = \cos A \cos B \mp \sin A \sin B$ $\tan(A \pm B) = \frac{\tan A \pm \tan B}{1 \mp \tan A \tan B} \qquad (A \pm B \neq (k + \frac{1}{2})\pi)$

Hyperbolic functions

$$\cosh^{2} x - \sinh^{2} x = 1$$

 $\sinh^{-1} x = \ln [x + \sqrt{(x^{2} + 1)}]$
 $\cosh^{-1} x = \ln [x + \sqrt{(x^{2} - 1)}], x \ge 1$

$$\tanh^{-1} x = \frac{1}{2} \ln \left(\frac{1+x}{1-x} \right), -1 < x < 1$$

Simple harmonic motion

$$x = A\cos(\omega t) + B\sin(\omega t)$$

 $x = R\sin(\omega t + \varphi)$

Statistics

Probability

$$P(A \cup B) = P(A) + P(B) - P(A \cap B)$$
$$P(A \cap B) = P(A)P(B|A) = P(B)P(A|B) \quad \text{or} \quad P(A|B) = \frac{P(A \cap B)}{P(B)}$$

Standard deviation

$$\sqrt{\frac{\Sigma(x-\overline{x})^2}{n}} = \sqrt{\frac{\Sigma x^2}{n} - \overline{x}^2}$$
 or $\sqrt{\frac{\Sigma f(x-\overline{x})^2}{\Sigma f}} = \sqrt{\frac{\Sigma f x^2}{\Sigma f} - \overline{x}^2}$

Sampling distributions

For any variable X, $E(\overline{X}) = \mu$, $Var(\overline{X}) = \frac{\sigma^2}{n}$ and \overline{X} is approximately normally distributed when *n* is large enough (approximately n > 25) If $X \sim N(\mu, \sigma^2)$ then $\overline{X} \sim N\left(\mu, \frac{\sigma^2}{n}\right)$ and $\frac{\overline{X} - \mu}{\sigma/\sqrt{n}} \sim N(0, 1)$

Unbiased estimates of the population mean and variance are given by $\frac{\sum x}{n}$ and $\frac{n}{n-1} \left(\frac{\sum x^2}{n} - \left(\frac{\sum x}{n} \right)^2 \right)$

Expectation algebra

Use the following results, including the cases where $a = b = \pm 1$ and/or c = 0:

- 1. E(aX+bY+c) = aE(X) + bE(Y) + c,
- 2. if *X* and *Y* are independent then $Var(aX+bY+c) = a^2 Var(X) + b^2 Var(Y)$.

Discrete distributions

X is a random variable taking values x_i in a discrete distribution with $P(X = x_i) = p_i$

Expectation: $\mu = E(X) = \sum x_i p_i$ Variance: $\sigma^2 = Var(X) = \sum (x_i - \mu)^2 p_i = \sum x_i^2 p_i - \mu^2$

	P(X = x)	$\mathrm{E}(X)$	Var(X)
Binomial $B(n, p)$	$\binom{n}{x} p^x (1-p)^{n-x}$	np	np(1-p)
Uniform distribution over 1, 2,, n , U(n)	$\frac{1}{n}$	$\frac{n+1}{2}$	$\frac{1}{12}(n^2-1)$
Geometric distribution Geo(<i>p</i>)	$(1-p)^{x-1}p$	$\frac{1}{p}$	$\frac{1-p}{p^2}$
Poisson $Po(\lambda)$	$e^{-\lambda} \frac{\lambda^x}{x!}$	λ	λ

Continuous distributions

X is a continuous random variable with probability density function (p.d.f.) f(x)

Expectation: $\mu = E(X) = \int x f(x) dx$ Variance: $\sigma^2 = Var(X) = \int (x-\mu)^2 f(x) dx = \int x^2 f(x) dx - \mu^2$ Cumulative distribution function $F(x) = P(X \le x) = \int_{-\infty}^{x} f(t) dt$

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	p.d.f.	$\mathrm{E}(X)$	$\operatorname{Var}(X)$
Continuous uniform distribution over $[a, b]$	$\frac{1}{b-a}$	$\frac{1}{2}(a+b)$	$\frac{1}{12}(b-a)^2$
Exponential	$\lambda e^{-\lambda x}$	$\frac{1}{\lambda}$	$\frac{1}{\lambda^2}$
Normal $N(\mu, \sigma^2)$	$\frac{1}{\sigma\sqrt{2\pi}}e^{-\frac{1}{2}\left(\frac{x-\mu}{\sigma}\right)^2}$	μ	σ^2

Percentage points of the normal distribution

If *Z* has a normal distribution with mean 0 and variance 1 then, for each value of *p*, the table gives the value of *z* such that $P(Z \le z) = p$.

p	0.75	0.90	0.95	0.975	0.99	0.995	0.9975	0.999	0.9995
z	0.674	1.282	1.645	1.960	2.326	2.576	2.807	3.090	3.291

Non-parametric tests

Goodness-of-fit test and contingency tables: $\sum \frac{(O_i - E_i)^2}{E_i} \sim \chi_v^2$

Approximate distributions for large samples

Wilcoxon Signed Rank test:
$$T \sim N\left(\frac{1}{4}n(n+1), \frac{1}{24}n(n+1)(2n+1)\right)$$

Wilcoxon Rank Sum test (samples of sizes *m* and *n*, with $m \le n$):

$$W \sim N\left(\frac{1}{2}m(m+n+1), \frac{1}{12}mn(m+n+1)\right)$$

Correlation and regression

For a sample of *n* pairs of observations (x_i, y_i)

$$S_{xx} = \sum (x_i - \overline{x})^2 = \sum x_i^2 - \frac{\left(\sum x_i\right)^2}{n}, \quad S_{yy} = \sum (y_i - \overline{y})^2 = \sum y_i^2 - \frac{\left(\sum y_i\right)^2}{n},$$
$$S_{xy} = \sum (x_i - \overline{x})(y_i - \overline{y}) = \sum x_i y_i - \frac{\sum x_i \sum y_i}{n}$$

Product moment correlation coefficient:
$$r = \frac{S_{xy}}{\sqrt{S_{xx}S_{yy}}} = \frac{\sum x_i y_i - \frac{\sum x_i \sum y_i}{n}}{\sqrt{\left[\left(\sum x_i^2 - \frac{\left(\sum x_i\right)^2}{n}\right)\left(\sum y_i^2 - \frac{\left(\sum y_i\right)^2}{n}\right)\right]}}$$

The regression coefficient of y on x is $b = \frac{S_{xy}}{S_{xx}} = \frac{\sum (x_i - \overline{x})(y_i - \overline{y})}{\sum (x_i - \overline{x})^2}$

Least squares regression line of y on x is y = a + bx where $a = \overline{y} - b\overline{x}$

Spearman's rank correlation coefficient: $r_s = 1 - \frac{6\sum d_i^2}{n(n^2 - 1)}$

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Critical values for the product moment correlation coefficient, r

Critical values for Spearman's rank correlation coefficient, r_s

											.		
	5%	21⁄2%	1%	1⁄2%	1- Т	Tail Test	5%	21⁄2%	1%	1⁄2%			
	10%	5%	2%	1%	2- Т	Tail Test	10%	5%	2%	1%			
п			7			п				7	Í	n	Î
1	-	-	-	-		31	0.3009	0.3550	0.4158	0.4556		1	I
2	-	-	-	-		32	0.2960	0.3494	0.4093	0.4487		2	I
3	0.9877	0.9969	0.9995	0.9999		33	0.2913	0.3440	0.4032	0.4421		3	
4	0.9000	0.9500	0.9800	0.9900		34	0.2869	0.3388	0.3972	0.4357		4	I
5	0.8054	0.8783	0.9343	0.9587		35	0.2826	0.3338	0.3916	0.4296		5	
6	0.7293	0.8114	0.8822	0.9172		36	0.2785	0.3291	0.3862	0.4238		6	Ī
7	0.6694	0.7545	0.8329	0.8745		37	0.2746	0.3246	0.3810	0.4182		7	
8	0.6215	0.7067	0.7887	0.8343		38	0.2709	0.3202	0.3760	0.4128		8	
9	0.5822	0.6664	0.7498	0.7977		39	0.2673	0.3160	0.3712	0.4076		9	
10	0.5494	0.6319	0.7155	0.7646		40	0.2638	0.3120	0.3665	0.4026		10	
11	0.5214	0.6021	0.6851	0.7348		41	0.2605	0.3081	0.3621	0.3978		11	Ī
12	0.4973	0.5760	0.6581	0.7079		42	0.2573	0.3044	0.3578	0.3932		12	I
13	0.4762	0.5529	0.6339	0.6835		43	0.2542	0.3008	0.3536	0.3887		13	I
14	0.4575	0.5324	0.6120	0.6614		44	0.2512	0.2973	0.3496	0.3843		14	I
15	0.4409	0.5140	0.5923	0.6411		45	0.2483	0.2940	0.3457	0.3801		15	
16	0.4259	0.4973	0.5742	0.6226		46	0.2455	0.2907	0.3420	0.3761		16	Ī
17	0.4124	0.4821	0.5577	0.6055		47	0.2429	0.2876	0.3384	0.3721		17	I
18	0.4000	0.4683	0.5425	0.5897		48	0.2403	0.2845	0.3348	0.3683		18	I
19	0.3887	0.4555	0.5285	0.5751		49	0.2377	0.2816	0.3314	0.3646		19	I
20	0.3783	0.4438	0.5155	0.5614		50	0.2353	0.2787	0.3281	0.3610		20	
21	0.3687	0.4329	0.5034	0.5487		51	0.2329	0.2759	0.3249	0.3575		21	Ī
22	0.3598	0.4227	0.4921	0.5368		52	0.2306	0.2732	0.3218	0.3542		22	I
23	0.3515	0.4132	0.4815	0.5256		53	0.2284	0.2706	0.3188	0.3509		23	
24	0.3438	0.4044	0.4716	0.5151		54	0.2262	0.2681	0.3158	0.3477		24	
25	0.3365	0.3961	0.4622	0.5052		55	0.2241	0.2656	0.3129	0.3445		25	I
26	0.3297	0.3882	0.4534	0.4958		56	0.2221	0.2632	0.3102	0.3415		26	Ī
27	0.3233	0.3809	0.4451	0.4869		57	0.2201	0.2609	0.3074	0.3385		27	I
28	0.3172	0.3739	0.4372	0.4785		58	0.2181	0.2586	0.3048	0.3357		28	Í
29	0.3115	0.3673	0.4297	0.4705		59	0.2162	0.2564	0.3022	0.3328		29	Í
30	0.3061	0.3610	0.4226	0.4629		60	0.2144	0.2542	0.2997	0.3301		30	Í
											1		1

10%5%2%1%2-Tail Test10%5%10%5%2%1%Test10%5%10%310.30120.3560320.29620.3504330.29140.34491.0000340.28710.33960.90001.00001.0000-360.27880.33070.82860.88570.94291.0000360.27880.33000.71430.78570.89290.9286370.27480.32530.64290.73810.83330.8810380.26140.31680.56360.64850.74550.7939400.26400.31280.55360.58740.67830.7273420.25740.30510.54350.56040.64840.7033430.25430.30140.46370.53850.62640.6791440.25130.29780.44640.52140.60360.6536450.24840.29130.44640.52140.56620.6176440.24030.28800.41420.48770.56620.6176450.22180.29130.41420.48670.55160.5588450.23280.27140.35050.44660.52180.5699550.23230.27140.35080.42520.49750.	5%	21/2%	1%	1⁄2%	1- Т	Tail Test	5%	21/2%
n n n - - - 31 0.3012 0.3560 - - - - 32 0.2962 0.3544 1.0000 - - - 33 0.2914 0.3449 1.0000 - - - 34 0.2871 0.3396 0.9000 1.0000 - - 36 0.2788 0.3300 0.7143 0.7857 0.8929 0.9286 37 0.2748 0.3253 0.6429 0.7381 0.8333 0.8810 38 0.2710 0.3209 0.6000 0.7000 0.7833 0.8333 39 0.2674 0.3168 0.5536 0.5874 0.6783 0.7273 41 0.2606 0.3087 0.4637 0.5385 0.6264 0.6791 444 0.2513 0.3014 0.4464 0.5291 0.5584 0.6353 45 0.2484 0.2993 0.3112 0.4566 </td <td>10%</td> <td>5%</td> <td>2%</td> <td>1%</td> <td>2- T</td> <td>Tail Test</td> <td>10%</td> <td>5%</td>	10%	5%	2%	1%	2- T	Tail Test	10%	5%
- - - - 31 0.3012 0.3560 - - - 32 0.2962 0.3504 1.0000 - - 33 0.2914 0.3499 0.9000 1.0000 - 34 0.2871 0.3396 0.9000 1.0000 - 36 0.2829 0.3347 0.8286 0.8857 0.9429 1.0000 36 0.2788 0.3300 0.7143 0.7857 0.8929 0.9286 37 0.2748 0.3253 0.6429 0.7381 0.8333 0.8810 38 0.2710 0.3209 0.6000 0.7000 0.7833 0.8333 39 0.2674 0.3188 0.5535 0.5644 0.6783 0.7273 42 0.2574 0.3014 0.4637 0.5385 0.6264 0.6791 44 0.2513 0.2978 0.4464 0.5291 0.5584 0.6536 45 0.2484 0.2913						п		
- - - - 32 0.2962 0.3504 1.0000 - - - 33 0.2914 0.3499 0.9000 1.0000 - - 34 0.2871 0.3396 0.8286 0.8857 0.9429 1.0000 - 36 0.2788 0.3300 0.7143 0.7857 0.8929 0.9286 37 0.2748 0.3209 0.6429 0.7381 0.8333 0.8810 38 0.2710 0.3209 0.6000 0.7000 0.7833 0.8333 39 0.2674 0.3168 0.5364 0.6182 0.7091 0.7545 41 0.2606 0.3087 0.4463 0.5604 0.6791 44 0.2513 0.3014 0.4464 0.5214 0.6036 0.6536 45 0.2484 0.2913 0.4142 0.4576 0.5218 0.5699 48 0.2403 0.2850 0.3305 0.4466 0.5218	-	-	-	-		31	0.3012	0.3560
- - - 33 0.2914 0.3449 1.0000 - - - 34 0.2871 0.336 0.8286 0.8857 0.9429 1.0000 35 0.2829 0.3347 0.8286 0.8857 0.9429 0.9286 37 0.2748 0.3253 0.6429 0.7381 0.8333 0.8810 38 0.2710 0.3209 0.6000 0.7000 0.7833 0.8333 39 0.2674 0.3168 0.5364 0.6182 0.7091 0.7545 41 0.2606 0.3087 0.5035 0.5874 0.6783 0.7273 42 0.2574 0.3051 0.4835 0.5604 0.6484 0.7033 43 0.2543 0.3014 0.4637 0.5385 0.6264 0.6791 44 0.2513 0.2978 0.4464 0.5029 0.5824 0.6353 46 0.2456 0.2913 0.4142 0.4476 0.5501	-	-	-	-		32	0.2962	0.3504
1.0000340.28710.33960.90001.00001.0000-350.28290.33470.82860.88570.94291.0000360.27880.33000.71430.78570.89290.9286370.27480.32530.64290.73810.83330.8810380.27100.32090.60000.70000.78330.8333390.26740.31680.56360.64850.74550.7939400.26400.31280.53640.61820.70910.7545410.26060.30870.50350.58740.67830.7273420.25740.30140.46370.53850.62640.6791440.25130.29780.44640.52140.60360.6536450.24840.29450.42940.50290.58240.6353460.24560.29130.41420.48770.56620.6176470.24290.28800.39120.45960.53510.5842490.23780.28200.38050.44660.52180.5699500.23530.27140.37010.43640.50910.5558510.22290.27640.36080.42520.49750.5438520.23070.27360.33660.39010.45710.5009540.22620.26550.33690.39770.46620.510855 <td< td=""><td>-</td><td>-</td><td>-</td><td>-</td><td></td><td>33</td><td>0.2914</td><td>0.3449</td></td<>	-	-	-	-		33	0.2914	0.3449
0.90001.0000-350.28290.33470.82860.88570.94291.0000360.27880.33000.71430.78570.89290.9286370.27480.32530.64290.73810.83330.8810380.27100.32090.60000.70000.78330.8333390.26740.31680.56360.64850.74550.7939400.26400.31280.53640.61820.70910.7545410.26060.30870.50350.58740.67830.7273420.25740.30510.48350.56040.64840.7033430.25430.30140.46370.53850.62640.6791440.25130.29780.44640.52140.60360.6536450.24840.29450.41420.48770.56620.6176470.24290.28800.40140.47160.55010.5996480.24030.28500.39120.45960.53510.5842490.23780.28200.36080.42520.49750.5438520.23070.27640.35280.41600.48620.5108550.22420.26590.33060.39010.45710.5009540.22620.26350.33690.39770.46620.5108550.22420.26360.31800.37550.44010.482858 <td< td=""><td>1.0000</td><td>-</td><td>-</td><td>-</td><td></td><td>34</td><td>0.2871</td><td>0.3396</td></td<>	1.0000	-	-	-		34	0.2871	0.3396
0.8286 0.8857 0.9429 1.0000 36 0.2788 0.3300 0.7143 0.7857 0.8929 0.9286 37 0.2748 0.3253 0.6429 0.7381 0.8333 0.8810 38 0.2710 0.3209 0.6000 0.7000 0.7833 0.8333 39 0.2674 0.3168 0.5536 0.6485 0.7455 0.7939 40 0.2600 0.3087 0.5035 0.5874 0.6783 0.7273 42 0.2574 0.3051 0.4835 0.5604 0.6484 0.7033 43 0.2543 0.3014 0.4637 0.5385 0.6264 0.6791 44 0.2513 0.2978 0.4464 0.5214 0.6036 0.6536 45 0.2484 0.2945 0.4142 0.4877 0.5662 0.6176 47 0.2429 0.2880 0.3912 0.4596 0.5351 0.5842 49 0.2378 0.2820 0.3608 <td>0.9000</td> <td>1.0000</td> <td>1.0000</td> <td>-</td> <td></td> <td>35</td> <td>0.2829</td> <td>0.3347</td>	0.9000	1.0000	1.0000	-		35	0.2829	0.3347
0.7143 0.7857 0.8929 0.9286 37 0.2748 0.3253 0.6429 0.7381 0.8333 0.8810 38 0.2710 0.3209 0.6000 0.7000 0.7833 0.8333 0.8333 39 0.2674 0.3168 0.5636 0.6485 0.7455 0.7939 40 0.2600 0.3087 0.5035 0.5874 0.6783 0.7273 42 0.2574 0.3051 0.4835 0.5604 0.6484 0.7033 43 0.2543 0.3014 0.4637 0.5385 0.6264 0.6791 44 0.2513 0.2978 0.4464 0.5214 0.6036 0.6536 45 0.2484 0.2945 0.4142 0.4877 0.5662 0.6176 47 0.2429 0.2880 0.4014 0.4716 0.5501 0.5996 48 0.2403 0.2850 0.3805 0.4466 0.5218 0.5699 50 0.2353 0.2764 0.3608 0.4252 0.4975 0.5438 52 0.2307 0.2736	0.8286	0.8857	0.9429	1.0000		36	0.2788	0.3300
0.64290.73810.83330.8810380.27100.32090.60000.70000.78330.8333390.26740.31680.56360.64850.74550.7939400.26400.31280.53640.61820.70910.7545410.26060.30870.50350.58740.67830.7273420.25740.30140.48350.56040.64840.7033430.25430.30140.46370.53850.62640.6791440.25130.29780.44640.52140.60360.6536450.24840.29450.41420.48770.56620.6176470.24290.28800.40140.47160.55010.5996480.24030.28500.39120.45660.52180.5699500.23530.27910.37010.43640.50910.5558510.23290.27640.36080.42520.49750.5438520.23070.27360.33690.39070.46620.5108550.22420.26850.33690.39770.46620.5108560.22210.26360.31800.37550.44010.4828580.21810.25890.31180.36850.43250.4749590.21620.25670.30630.36240.42510.4670600.21440.2545	0.7143	0.7857	0.8929	0.9286		37	0.2748	0.3253
0.60000.70000.78330.8333390.26740.31680.56360.64850.74550.7939400.26400.31280.53640.61820.70910.7545410.26060.30870.50350.58740.67830.7273420.25740.30140.48350.56040.64840.7033430.25430.30140.46370.53850.62640.6791440.25130.29780.44640.52140.60360.6536450.24840.29450.42940.50290.58240.6353460.24560.29130.41420.48770.56620.6176470.24290.28800.40140.47160.55010.5996480.24030.28500.39120.45960.53510.5842490.23780.28200.38050.44660.52180.5699500.23530.27910.37010.43640.50910.5558510.22840.27100.37030.44660.48620.5316530.22840.27100.33690.39770.46620.5108550.22420.26590.33690.39770.46620.5108550.22420.26590.31800.37550.44010.4828580.21810.25890.31180.36850.43250.4749590.21620.25670.30630.36240.42510.467	0.6429	0.7381	0.8333	0.8810		38	0.2710	0.3209
0.5636 0.6485 0.7455 0.7939 40 0.2640 0.3128 0.5364 0.6182 0.7091 0.7545 41 0.2606 0.3087 0.5035 0.5874 0.6783 0.7273 42 0.2574 0.3051 0.4835 0.5604 0.6484 0.7033 43 0.2543 0.3014 0.4637 0.5385 0.6264 0.6791 44 0.2513 0.2978 0.4464 0.5214 0.6036 0.6536 45 0.2484 0.2945 0.4294 0.5029 0.5824 0.6353 46 0.2456 0.2913 0.4142 0.4877 0.5662 0.6176 47 0.2429 0.2880 0.4014 0.4716 0.5501 0.5996 48 0.2403 0.2850 0.3912 0.4596 0.53151 0.5842 49 0.2378 0.2820 0.3805 0.4466 0.5218 0.5699 50 0.2353 0.2791 0.3701 0.4364 0.5091 0.5558 51 0.2329 0.2764 0.368 0.4252 0.4975 0.5438 52 0.2307 0.2736 0.3369 0.3907 0.4662 0.5108 55 0.2242 0.2685 0.3366 0.3901 0.4571 0.5009 56 0.2221 0.2636 0.3180 0.3755 0.4401 0.4828 58 0.2181 0.2589 0.3118 0.3624 0.4251 <td>0.6000</td> <td>0.7000</td> <td>0.7833</td> <td>0.8333</td> <td></td> <td>39</td> <td>0.2674</td> <td>0.3168</td>	0.6000	0.7000	0.7833	0.8333		39	0.2674	0.3168
0.53640.61820.70910.7545410.26060.30870.50350.58740.67830.7273420.25740.30510.48350.56040.64840.7033430.25430.30140.46370.53850.62640.6791440.25130.29780.44640.52140.60360.6536450.24840.29450.42940.50290.58240.6353460.24560.29130.41420.48770.56620.6176470.24290.28800.40140.47160.55010.5996480.24030.28500.39120.45960.53510.5842490.23780.28200.38050.44660.52180.5699500.23530.27910.37010.43640.50910.5558510.23290.27640.36080.42520.49750.5438520.23070.27360.35280.41600.48620.5108550.22420.26590.33690.39770.46620.5108550.22420.26590.33060.39010.45710.5009560.22210.26360.31800.37550.44010.4828580.21810.25890.31180.36850.43250.4749590.21620.25670.30630.36240.42510.4670600.21440.2545	0.5636	0.6485	0.7455	0.7939		40	0.2640	0.3128
0.50350.58740.67830.7273420.25740.30510.48350.56040.64840.7033430.25430.30140.46370.53850.62640.6791440.25130.29780.44640.52140.60360.6536450.24840.29150.42940.50290.58240.6353460.24560.29130.41420.48770.56620.6176470.24290.28800.40140.47160.55010.5996480.24030.28500.39120.45960.53510.5842490.23780.28200.38050.44660.52180.5699500.23530.27910.37010.43640.50910.5558510.22840.27100.36080.42520.49750.5438520.23070.27360.33690.39770.46620.5108550.22420.26590.33060.39010.45710.5009540.22620.26850.31800.37550.44010.4828580.21810.25890.31180.36850.43250.4749590.21620.25670.30630.36240.42510.4670600.21440.2545	0.5364	0.6182	0.7091	0.7545		41	0.2606	0.3087
0.48350.56040.64840.7033430.25430.30140.46370.53850.62640.6791440.25130.29780.44640.52140.60360.6536450.24840.29450.42940.50290.58240.6353460.24560.29130.41420.48770.56620.6176470.24290.28800.40140.47160.55010.5996480.24030.28500.39120.45960.53510.5842490.23780.28200.38050.44660.52180.5699500.23530.27910.37010.43640.50910.5558510.23290.27640.36080.42520.49750.5438520.23070.27360.33690.39770.46620.5108550.22420.26590.33060.39010.45710.5009560.22210.26360.31800.37550.44010.4828580.21810.25890.31180.36850.43250.4749590.21620.25670.30630.36240.42510.4670600.21440.2545	0.5035	0.5874	0.6783	0.7273		42	0.2574	0.3051
0.4637 0.5385 0.6264 0.6791 44 0.2513 0.2978 0.4464 0.5214 0.6036 0.6536 45 0.2484 0.2945 0.4294 0.5029 0.5824 0.6353 46 0.2456 0.2913 0.4142 0.4877 0.5662 0.6176 47 0.2429 0.2880 0.4014 0.4716 0.5501 0.5996 48 0.2403 0.2850 0.3912 0.4596 0.5351 0.5842 49 0.2378 0.2820 0.3805 0.4466 0.5218 0.5699 50 0.2353 0.2791 0.3701 0.4364 0.5091 0.5558 51 0.2307 0.2736 0.3608 0.4252 0.4975 0.5438 52 0.2307 0.2736 0.3443 0.4070 0.4757 0.5209 54 0.2262 0.2685 0.3369 0.3977 0.4662 0.5108 55 0.2242 0.2659 0.3306 0.3901 0.4571 0.5009 56 0.2221 0.2636 <t< td=""><td>0.4835</td><td>0.5604</td><td>0.6484</td><td>0.7033</td><td></td><td>43</td><td>0.2543</td><td>0.3014</td></t<>	0.4835	0.5604	0.6484	0.7033		43	0.2543	0.3014
0.4464 0.5214 0.6036 0.6536 45 0.2484 0.2945 0.4294 0.5029 0.5824 0.6353 46 0.2456 0.2913 0.4142 0.4877 0.5662 0.6176 47 0.2429 0.2880 0.4014 0.4716 0.5501 0.5996 48 0.2403 0.2850 0.3912 0.4596 0.5351 0.5842 49 0.2378 0.2820 0.3805 0.4466 0.5218 0.5699 50 0.2353 0.2791 0.3701 0.4364 0.5091 0.5558 51 0.2329 0.2764 0.3608 0.4252 0.4975 0.5438 52 0.2307 0.2736 0.3528 0.4160 0.4862 0.5316 53 0.2284 0.2710 0.3443 0.4070 0.4757 0.5209 54 0.2262 0.2659 0.3369 0.3901 0.4571 0.5009 56 0.2221 0.2656 0.3180 <td>0.4637</td> <td>0.5385</td> <td>0.6264</td> <td>0.6791</td> <td></td> <td>44</td> <td>0.2513</td> <td>0.2978</td>	0.4637	0.5385	0.6264	0.6791		44	0.2513	0.2978
0.42940.50290.58240.6353460.24560.29130.41420.48770.56620.6176470.24290.28800.40140.47160.55010.5996480.24030.28500.39120.45960.53510.5842490.23780.28200.38050.44660.52180.5699500.23530.27910.37010.43640.50910.5558510.23290.27640.36080.42520.49750.5438520.23070.27360.35280.41600.48620.5316530.22840.27100.34430.40700.47570.5209540.22620.26850.33690.39770.46620.5108550.22420.26590.33060.39010.45710.5009560.22210.26360.31800.37550.44010.4828580.21810.25890.31180.36850.43250.4749590.21620.25670.30630.36240.42510.4670600.21440.2545	0.4464	0.5214	0.6036	0.6536		45	0.2484	0.2945
0.4142 0.4877 0.5662 0.6176 47 0.2429 0.2880 0.4014 0.4716 0.5501 0.5996 48 0.2403 0.2850 0.3912 0.4596 0.5351 0.5842 49 0.2378 0.2820 0.3805 0.4466 0.5218 0.5699 50 0.2353 0.2791 0.3701 0.4364 0.5091 0.5558 51 0.2329 0.2764 0.3608 0.4252 0.4975 0.5438 52 0.2307 0.2736 0.3528 0.4160 0.4862 0.5316 53 0.2284 0.2710 0.3443 0.4070 0.4757 0.5209 54 0.2262 0.2685 0.3369 0.3977 0.4662 0.5108 55 0.2242 0.2659 0.3306 0.3901 0.4571 0.5009 56 0.2221 0.2636 0.3242 0.3828 0.4487 0.4915 57 0.2201 0.2612 0.3180 0.3755 0.4401 0.4828 58 0.2181 0.2589 <t< td=""><td>0.4294</td><td>0.5029</td><td>0.5824</td><td>0.6353</td><td></td><td>46</td><td>0.2456</td><td>0.2913</td></t<>	0.4294	0.5029	0.5824	0.6353		46	0.2456	0.2913
0.4014 0.4716 0.5501 0.5996 48 0.2403 0.2850 0.3912 0.4596 0.5351 0.5842 49 0.2378 0.2820 0.3805 0.4466 0.5218 0.5699 50 0.2353 0.2791 0.3701 0.4364 0.5091 0.5558 51 0.2307 0.2736 0.3608 0.4252 0.4975 0.5438 52 0.2307 0.2736 0.3528 0.4160 0.4862 0.5316 53 0.2284 0.2710 0.3443 0.4070 0.4757 0.5209 54 0.2262 0.2685 0.3369 0.3977 0.4662 0.5108 55 0.2242 0.2659 0.3306 0.3901 0.4571 0.5009 56 0.2221 0.2636 0.3242 0.3828 0.4487 0.4915 57 0.2201 0.2612 0.3180 0.3755 0.4401 0.4828 58 0.2181 0.2589 0.3118 0.3624 0.4251 0.4670 60 0.2144 0.2545 <td>0.4142</td> <td>0.4877</td> <td>0.5662</td> <td>0.6176</td> <td></td> <td>47</td> <td>0.2429</td> <td>0.2880</td>	0.4142	0.4877	0.5662	0.6176		47	0.2429	0.2880
0.3912 0.4596 0.5351 0.5842 49 0.2378 0.2820 0.3805 0.4466 0.5218 0.5699 50 0.2353 0.2791 0.3701 0.4364 0.5091 0.5558 51 0.2329 0.2764 0.3608 0.4252 0.4975 0.5438 52 0.2307 0.2736 0.3528 0.4160 0.4862 0.5316 53 0.2284 0.2710 0.3443 0.4070 0.4757 0.5209 54 0.2262 0.2685 0.3369 0.3977 0.4662 0.5108 55 0.2242 0.2659 0.3306 0.3901 0.4571 0.5009 56 0.2221 0.2636 0.3242 0.3828 0.4487 0.4915 57 0.2201 0.2612 0.3180 0.3755 0.4401 0.4828 58 0.2181 0.2589 0.3118 0.3685 0.4325 0.4749 59 0.2162 0.2567 0.3063 0.3624 0.4251 0.4670 60 0.2144 0.2545 <td>0.4014</td> <td>0.4716</td> <td>0.5501</td> <td>0.5996</td> <td></td> <td>48</td> <td>0.2403</td> <td>0.2850</td>	0.4014	0.4716	0.5501	0.5996		48	0.2403	0.2850
0.3805 0.4466 0.5218 0.5699 50 0.2353 0.2791 0.3701 0.4364 0.5091 0.5558 51 0.2329 0.2764 0.3608 0.4252 0.4975 0.5438 52 0.2307 0.2736 0.3528 0.4160 0.4862 0.5316 53 0.2284 0.2710 0.3443 0.4070 0.4757 0.5209 54 0.2262 0.2685 0.3369 0.3977 0.4662 0.5108 55 0.2242 0.2659 0.3306 0.3901 0.4571 0.5009 56 0.2221 0.2636 0.3242 0.3828 0.4487 0.4915 57 0.2201 0.2612 0.3180 0.3755 0.4401 0.4828 58 0.2181 0.2589 0.3118 0.3685 0.4325 0.4749 59 0.2162 0.2567 0.3063 0.3624 0.4251 0.4670 60 0.2144 0.2545	0.3912	0.4596	0.5351	0.5842		49	0.2378	0.2820
0.3701 0.4364 0.5091 0.5558 51 0.2329 0.2764 0.3608 0.4252 0.4975 0.5438 52 0.2307 0.2736 0.3528 0.4160 0.4862 0.5316 53 0.2284 0.2710 0.3443 0.4070 0.4757 0.5209 54 0.2262 0.2685 0.3369 0.3977 0.4662 0.5108 55 0.2242 0.2659 0.3306 0.3901 0.4571 0.5009 56 0.2221 0.2636 0.3242 0.3828 0.4487 0.4915 57 0.2201 0.2612 0.3180 0.3755 0.4401 0.4828 58 0.2181 0.2589 0.3118 0.3685 0.4325 0.4749 59 0.2162 0.2567 0.3063 0.3624 0.4251 0.4670 60 0.2144 0.2545	0.3805	0.4466	0.5218	0.5699		50	0.2353	0.2791
0.3608 0.4252 0.4975 0.5438 52 0.2307 0.2736 0.3528 0.4160 0.4862 0.5316 53 0.2284 0.2710 0.3443 0.4070 0.4757 0.5209 54 0.2262 0.2685 0.3369 0.3977 0.4662 0.5108 55 0.2242 0.2659 0.3306 0.3901 0.4571 0.5009 56 0.2221 0.2636 0.3242 0.3828 0.4487 0.4915 57 0.2201 0.2612 0.3180 0.3755 0.4401 0.4828 58 0.2181 0.2589 0.3118 0.3685 0.4325 0.4749 59 0.2162 0.2567 0.3063 0.3624 0.4251 0.4670 60 0.2144 0.2545	0.3701	0.4364	0.5091	0.5558		51	0.2329	0.2764
0.3528 0.4160 0.4862 0.5316 53 0.2284 0.2710 0.3443 0.4070 0.4757 0.5209 54 0.2262 0.2685 0.3369 0.3977 0.4662 0.5108 55 0.2242 0.2659 0.3306 0.3901 0.4571 0.5009 56 0.2221 0.2636 0.3242 0.3828 0.4487 0.4915 57 0.2201 0.2612 0.3180 0.3755 0.4401 0.4828 58 0.2181 0.2589 0.3118 0.3685 0.4325 0.4749 59 0.2162 0.2567 0.3063 0.3624 0.4251 0.4670 60 0.2144 0.2545	0.3608	0.4252	0.4975	0.5438		52	0.2307	0.2736
0.3443 0.4070 0.4757 0.5209 54 0.2262 0.2685 0.3369 0.3977 0.4662 0.5108 55 0.2242 0.2659 0.3306 0.3901 0.4571 0.5009 56 0.2221 0.2636 0.3242 0.3828 0.4487 0.4915 57 0.2201 0.2612 0.3180 0.3755 0.4401 0.4828 58 0.2181 0.2589 0.3118 0.3685 0.4325 0.4749 59 0.2162 0.2567 0.3063 0.3624 0.4251 0.4670 60 0.2144 0.2545	0.3528	0.4160	0.4862	0.5316		53	0.2284	0.2710
0.3369 0.3977 0.4662 0.5108 55 0.2242 0.2659 0.3306 0.3901 0.4571 0.5009 56 0.2221 0.2636 0.3242 0.3828 0.4487 0.4915 57 0.2201 0.2612 0.3180 0.3755 0.4401 0.4828 58 0.2181 0.2589 0.3118 0.3685 0.4325 0.4749 59 0.2162 0.2567 0.3063 0.3624 0.4251 0.4670 60 0.2144 0.2545	0.3443	0.4070	0.4757	0.5209		54	0.2262	0.2685
0.33060.39010.45710.5009560.22210.26360.32420.38280.44870.4915570.22010.26120.31800.37550.44010.4828580.21810.25890.31180.36850.43250.4749590.21620.25670.30630.36240.42510.4670600.21440.2545	0.3369	0.3977	0.4662	0.5108		55	0.2242	0.2659
0.32420.38280.44870.4915570.22010.26120.31800.37550.44010.4828580.21810.25890.31180.36850.43250.4749590.21620.25670.30630.36240.42510.4670600.21440.2545	0.3306	0.3901	0.4571	0.5009		56	0.2221	0.2636
0.31800.37550.44010.4828580.21810.25890.31180.36850.43250.4749590.21620.25670.30630.36240.42510.4670600.21440.2545	0.3242	0.3828	0.4487	0.4915		57	0.2201	0.2612
0.31180.36850.43250.4749590.21620.25670.30630.36240.42510.4670600.21440.2545	0.3180	0.3755	0.4401	0.4828		58	0.2181	0.2589
0.3063 0.3624 0.4251 0.4670 60 0.2144 0.2545	0.3118	0.3685	0.4325	0.4749		59	0.2162	0.2567
	0.3063	0.3624	0.4251	0.4670		60	0.2144	0.2545

 $\boldsymbol{\infty}$

1%

2%

0.4117

0.4054

0.3995

0.3936

0.3882

0.3829

0.3778

0.3729

0.3681

0.3636

0.3594

0.3550

0.3511

0.3470

0.3433

0.3396

0.3361

0.3326

0.3293

0.3260

0.3228

0.3198

0.3168

0.3139

0.3111

0.3083

0.3057

0.3030

0.3005 0.3314

0.4185 0.4593

1⁄2%

1%

0.4523

0.4455

0.4390

0.4328 0.4268

0.4211

0.4155

0.4103

0.4051

0.4002

0.3955

0.3908

0.3865

0.3822

0.3781

0.3741

0.3702

0.3664

0.3628

0.3592

0.3558

0.3524

0.3492

0.3460

0.3429

0.3400

0.3370

0.3342

Critical values for the χ^2 distribution

If *X* has a χ^2 distribution with *v* degrees of freedom then, for each pair of values of *p* and *v*, the table gives the value of *x* such that

$$\mathbf{P}(X \le x) = p.$$



р	0.01	0.025	0.05	0.90	0.95	0.975	0.99	0.995	0.999
v = 1	0.0 ³ 1571	0.0 ³ 9821	0.0 ² 3932	2.706	3.841	5.024	6.635	7.879	10.83
2	0.02010	0.05064	0.1026	4.605	5.991	7.378	9.210	10.60	13.82
3	0.1148	0.2158	0.3518	6.251	7.815	9.348	11.34	12.84	16.27
4	0.2971	0.4844	0.7107	7.779	9.488	11.14	13.28	14.86	18.47
5	0.5542	0.0210	1 1 4 5	0.226	11.07	10.02	15.00	1675	20.51
	0.3345	1.027	1.143	9.230	11.07	12.85	15.09	10.73	20.31
	1 220	1.237	2.167	10.04	12.39	14.45	10.01	10.33	22.40
0	1.239	2 1 2 0	2.107	12.02	14.07	17.52	20.00	20.20	24.52
	2.099	2.160	2.755	13.30	15.51	17.55	20.09	21.95	20.12
9	2.088	2.700	5.525	14.08	10.92	19.02	21.07	25.39	27.00
10	2.558	3.247	3.940	15.99	18.31	20.48	23.21	25.19	29.59
11	3.053	3.816	4.575	17.28	19.68	21.92	24.73	26.76	31.26
12	3.571	4.404	5.226	18.55	21.03	23.34	26.22	28.30	32.91
13	4.107	5.009	5.892	19.81	22.36	24.74	27.69	29.82	34.53
14	4.660	5.629	6.571	21.06	23.68	26.12	29.14	31.32	36.12
15	5 220	6 262	7 261	22.21	25.00	27.40	20.59	22.80	27 70
15	5.229	0.202	7.201	22.51	25.00	27.49	30.38 22.00	52.80 24.27	37.70 20.25
10	5.812	0.908	7.902 9.672	25.54	20.50	20.03	52.00 22.41	54.27 25.72	39.23 40.70
1/	0.408	7.304 9.321	8.072	24.77	27.59	30.19 21.52	24.91	33.72 27.16	40.79
18	7.015	8.231	9.390	25.99	28.87	31.33 22.95	54.81 26.10	37.10 20.50	42.51
19	/.033	8.907	10.12	27.20	30.14	52.85	30.19	38.38	43.82
20	8.260	9.591	10.85	28.41	31.41	34.17	37.57	40.00	45.31
21	8.897	10.28	11.59	29.62	32.67	35.48	38.93	41.40	46.80
22	9.542	10.98	12.34	30.81	33.92	36.78	40.29	42.80	48.27
23	10.20	11.69	13.09	32.01	35.17	38.08	41.64	44.18	49.73
24	10.86	12.40	13.85	33.20	36.42	39.36	42.98	45.56	51.18
25	11.50	12.10	14 61	24.20	27 65	10.65	44.21	46.02	50 (0
25	11.52	15.12	14.01	34.38	37.05	40.65	44.31	40.93	52.62
30	14.95	16.79	18.49	40.26	43.77	46.98	50.89	55.07	59.70
40	22.16	24.43	26.51	51.81	55.76	59.34	63.69	66.//	/3.40
50	29.71	32.36	34.76	63.17	67.50	/1.42	/6.15	/9.49	86.66
60	57.48	40.48	43.19	/4.40	/9.08	83.30	88.38	91.95	99.61
70	45.44	48.76	51.74	85.53	90.53	95.02	100.4	104.2	112.3
80	53.54	57.15	60.39	96.58	101.9	106.6	112.3	116.3	124.8
90	61.75	65.65	69.13	107.6	113.1	118.1	124.1	128.3	137.2
100	70.06	74.22	77.93	118.5	124.3	129.6	135.8	140.2	149.4

Wilcoxon signed rank test

 $W_{\rm +}$ is the sum of the ranks corresponding to the positive differences,

 W_{-} is the sum of the ranks corresponding to the negative differences,

T is the smaller of W_+ and W_- .

For each value of n the table gives the **largest** value of T which will lead to rejection of the null hypothesis at the level of significance indicated.

		Level of significance								
One Tail	0.05	0.025	0.01	0.005						
Two Tail	0.10	0.05	0.02	0.01						
<i>n</i> = 6	2	0								
7	3	2	0							
8	5	3	1	0						
9	8	5	3	1						
10	10	8	5	3						
11	13	10	7	5						
12	17	13	9	7						
13	21	17	12	9						
14	25	21	15	12						
15	30	25	19	15						
16	35	29	23	19						
17	41	34	27	23						
18	47	40	32	27						
19	53	46	37	32						
20	60	52	43	37						

Critical values of T

For larger values of *n*, each of W_+ and W_- can be approximated by the normal distribution with mean $\frac{1}{4}n(n+1)$ and variance $\frac{1}{24}n(n+1)(2n+1)$.

Wilcoxon rank sum test

The two samples have sizes *m* and *n*, where $m \le n$.

 R_m is the sum of the ranks of the items in the sample of size m.

W is the smaller of R_m and $m(m+n+1) - R_m$.

For each pair of values of *m* and *n*, the table gives the **largest** value of *W* which will lead to rejection of the null hypothesis at the level of significance indicated.

		Level of significance										
One Tail	0.05	0.025	0.01	0.05	0.025	0.01	0.05	0.025	0.01	0.05	0.025	0.01
Two Tail	0.1	0.05	0.02	0.1	0.05	0.02	0.1	0.05	0.02	0.1	0.05	0.02
п		<i>m</i> = 3			m = 4			<i>m</i> = 5			m = 6	
3	6	-	-									
4	6	-	-	11	10	-						
5	7	6	-	12	11	10	19	17	16			
6	8	7	-	13	12	11	20	18	17	28	26	24
7	8	7	6	14	13	11	21	20	18	29	27	25
8	9	8	6	15	14	12	23	21	19	31	29	27
9	10	8	7	16	14	13	24	22	20	33	31	28
10	10	9	7	17	15	13	26	23	21	35	32	29

	Level of significance											
One Tail	0.05	0.025	0.01	0.05	0.025	0.01	0.05	0.025	0.01	0.05	0.025	0.01
Two Tail	0.1	0.05	0.02	0.1	0.05	0.02	0.1	0.05	0.02	0.1	0.05	0.02
n	m = 7			m = 8			m = 9			m = 10		
7	39	36	34									
8	41	38	35	51	49	45						
9	43	40	37	54	51	47	66	62	59			
10	45	42	39	56	53	49	69	65	61	82	78	74

For larger values of *m* and *n*, the normal distribution with mean $\frac{1}{2}m(m+n+1)$ and variance $\frac{1}{12}mn(m+n+1)$ should be used as an approximation to the distribution of R_m .

Mechanics

Kinematics

Motion in a straight line

Motion in two dimensions

$$v = u + at$$
 $v = u + at$ $s = ut + \frac{1}{2}at^2$ $s = ut + \frac{1}{2}at^2$ $s = \frac{1}{2}(u + v)t$ $s = \frac{1}{2}(u + v)t$ $v^2 = u^2 + 2as$ $v \cdot v = u \cdot u + 2a \cdot s$ $s = vt - \frac{1}{2}at^2$ $s = vt - \frac{1}{2}at^2$

Newton's experimental law

Between two smooth spheres $v_1 - v_2 = -e(u_1 - u_2)$

Between a smooth sphere with a fixed plane surface v = -eu

Motion in a circle

Tangential velocity is $v = r\dot{\theta}$ Radial acceleration is $\frac{v^2}{r}$ or $r\dot{\theta}^2$ towards the centre Tangential acceleration is $\dot{v} = r\ddot{\theta}$

Centres of mass

Triangular lamina: $\frac{2}{3}$ along median from vertex Solid hemisphere, radius r: $\frac{3}{8}r$ from centre Hemispherical shell, radius r: $\frac{1}{2}r$ from centre Circular arc, radius r, angle at centre 2α : $\frac{r \sin \alpha}{\alpha}$ from centre Sector of circle, radius r, angle at centre 2α : $\frac{2r \sin \alpha}{3\alpha}$ from centre Solid cone or pyramid of height h: $\frac{1}{4}h$ above the base on the line from centre of base to vertex Conical shell of height h: $\frac{1}{3}h$ above the base on the line from centre of base to vertex

Discrete Mathematics

Inclusion-exclusion principle

For sets *A*, *B* and *C*:

 $n(A \cup B \cup C) = n(A) + n(B) + n(C) - n(A \cap B) - n(A \cap C) - n(B \cap C) + n(A \cap B \cap C)$

The hierarchy of orders

 $O(1) \subseteq O(\log n) \subseteq O(n) \subseteq O(n \log n) \subseteq O(n^2) \subseteq O(n^3) \subseteq \ldots \subseteq O(a^n) \subseteq O(n!)$

Sorting algorithms

Bubble sort:

Start at the left hand end of the list unless specified otherwise.

Compare the first and second values and swap if necessary. Then compare the (new) second value with the third value and swap if necessary. Continue in this way until all values have been considered.

Fix the last value then repeat with the reduced list until either there is a pass in which no swaps occur or the list is reduced to length 1, then stop.

Shuttle sort:

Start at the left hand end of the list unless specified otherwise.

Compare the second value with the first and swap if necessary, this completes the first pass. Next compare the third value with the second and swap if necessary, if a swap happened shuttle back to compare the (new) second with the first as in the first pass, this completes the second pass.

Next compare the fourth value with the third and swap if necessary, if a swap happened shuttle back to compare the (new) third value with the second as in the second pass (so if a swap happens shuttle back again). Continue in this way for n-1 passes, where *n* is the length of the list.

Quick sort:

The first value in any sublist will be the pivot, unless specified otherwise.

Working from left to right, write down each value that is smaller than the pivot, then the pivot, then work along the list and write down each value that is not smaller than the pivot. This produces two sublists (one of which may be empty) with the pivot between them and completes the pass.

Next apply this procedure to each of the sublists from the previous pass, unless they consist of a single entry, to produce further sublists. Continue in this way until no sublist has more than one entry.

Network algorithms

Dijkstra's algorithm

- START with a graph *G*. At each vertex draw a box, the lower area for temporary labels, the upper left hand area for the order of becoming permanent and the upper right hand area for the permanent label.
- STEP 1 Make the given start vertex permanent by giving it permanent label 0 and order label 1.
- STEP 2 For each vertex that is not permanent and is connected by an arc to the vertex that has just been made permanent (with permanent label = P), add the arc weight to P. If this is smaller than the best temporary label at the vertex, write this value as the new best temporary label.
- STEP 3 Choose the vertex that is not yet permanent which has the smallest best temporary label. If there is more than one such vertex, choose any one of them. Make this vertex permanent and assign it the next order label.
- STEP 4 If every vertex is now permanent, or if the target vertex is permanent, use 'trace back' to find the routes or route, then STOP; otherwise return to STEP 2.

Prim's algorithm (graphical version)

START with an arbitrary vertex of *G*.

- STEP 1 Add an edge of minimum weight joining a vertex already included to a vertex not already included.
- STEP 2 If a spanning tree is obtained STOP; otherwise return to STEP 1.

Prim's algorithm (tabular version)

START with a table (or matrix) of weights for a connected weighted graph.

- STEP 1 Cross through the entries in an arbitrary row, and mark the corresponding column.
- STEP 2 Choose a minimum entry from the uncircled entries in the marked column(s).
- STEP 3 If no such entry exists STOP; otherwise go to STEP 4.
- STEP 4 Circle the weight w_{ii} found in STEP 2; mark column *i*; cross through row *i*.

STEP 5 Return to STEP 2.

Kruskal's algorithm

START with all the vertices of G, but no edges; list the edges in increasing order of weight.

- STEP 1 Add an edge of G of minimum weight in such a way that no cycles are created.
- STEP 2 If a spanning tree is obtained STOP; otherwise return to STEP 1.

Nearest neighbour method

START at a given vertex of *G*.

- STEP 1 Find the least weight arc from this vertex to a vertex that has not already been included (or back to the start vertex if every vertex has been included).
- STEP 2 If no such arc exists then the method has stalled STOP; otherwise add this arc to the path.
- STEP 3 If a cycle has been found STOP; otherwise return to STEP 1.

Lower bound for travelling salesperson problem

START with all vertices and arcs of G.

- STEP 1 Remove a given vertex and all arcs that are directly connected to that vertex, find a minimum spanning tree for the resulting reduced network.
- STEP 2 Add the weight of this minimum connector to the sum of the two least weight arcs that had been deleted. This gives a lower bound.

Route inspection problem

START with a list of the odd degree vertices.

- STEP 1 For each pair of odd nodes, find the connecting path of least weight.
- STEP 2 Group the odd nodes so that the sum of weights of the connecting paths is minimised.
- STEP 3 Add this sum to the total weight of the graph STOP.

The simplex algorithm

START with a tableau in standard format.

- STEP 1 Choose a column with a negative entry in the objective row (or zero in degenerate cases).
- STEP 2 The pivot row is the one for which non-negative value of the entry in the final column divided by the positive value of the entry in the pivot column is minimised. The pivot element is the entry of the pivot row in the chosen column.
- STEP 3 Divide all entries in the pivot row by the value of the pivot element.
- STEP 4 Add to, or subtract from, all other old rows a multiple of the new pivot row, so that the pivot column ends up consisting of zeroes and a single one, and corresponds to the new basic variable.
- STEP 5 If the objective row has no negative entries STOP; otherwise return to STEP 1.

Additional Pure Mathematics

Vector product

 $\mathbf{a} \times \mathbf{b} = |\mathbf{a}| |\mathbf{b}| \sin \theta \hat{\mathbf{n}}$, where $\mathbf{a}, \mathbf{b}, \hat{\mathbf{n}}$, in that order, form a right-handed triple.

Surfaces

For 3-D surfaces given in the form z = f(x, y), the Hessian Matrix is given by

At a stationary point of the surface:

- 1. if $|\mathbf{H}| > 0$ and $f_{xx} > 0$, there is a (local) minimum;
- 2. if $|\mathbf{H}|>0$ and $f_{_{\!\mathcal{X}\!X}}<0,$ there is a (local) maximum;
- 3. if $|\mathbf{H}| < 0$ there is a saddle-point;
- 4. if $|\mathbf{H}| = 0$ then the nature of the stationary point cannot be determined by this test.

The equation of a tangent plane to the curve at a given point (x, y, z) = (a, b, f(a, b)) is

$$z = f(a, b) + (x - a)f_{x}(a, b) + (y - b)f_{y}(a, b)$$

Calculus

Arc length

$$\int_{a}^{b} \sqrt{(\dot{x}^{2} + \dot{y}^{2})} dt$$
$$s = \int_{a}^{b} \sqrt{(\dot{x}^{2} + \dot{y}^{2})} dt$$

 $s = \int_{a}^{b} \sqrt{1 + \left(\frac{\mathrm{d}y}{\mathrm{d}x}\right)^2} \mathrm{d}x$

Surface area of revolution

$$S_{x} = 2\pi \int_{a}^{b} y \sqrt{1 + \left(\frac{\mathrm{d}y}{\mathrm{d}x}\right)^{2}} \,\mathrm{d}x \qquad \qquad S_{y} = 2\pi \int_{c}^{d} x \sqrt{1 + \left(\frac{\mathrm{d}x}{\mathrm{d}y}\right)^{2}} \,\mathrm{d}y$$
$$S_{x} = 2\pi \int_{a}^{b} y(t) \sqrt{\left(\frac{\mathrm{d}x}{\mathrm{d}t}\right)^{2} + \left(\frac{\mathrm{d}y}{\mathrm{d}t}\right)^{2}} \,\mathrm{d}t \qquad \qquad S_{y} = 2\pi \int_{c}^{d} x(t) \sqrt{\left(\frac{\mathrm{d}x}{\mathrm{d}t}\right)^{2} + \left(\frac{\mathrm{d}y}{\mathrm{d}t}\right)^{2}} \,\mathrm{d}t$$

 $\mathbf{H} = \begin{pmatrix} \mathbf{f}_{xx} & \mathbf{f}_{xy} \\ \mathbf{f}_{yx} & \mathbf{f}_{yy} \end{pmatrix}.$